

Units & Dimensions.

SI units & U.S. Customary units.

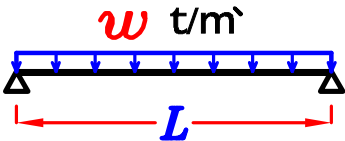
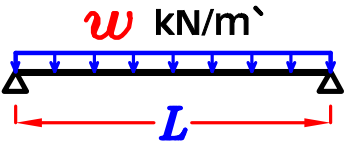
يوجد للتصميم في مصر نوعان من الوحدات:

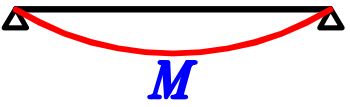
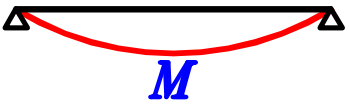
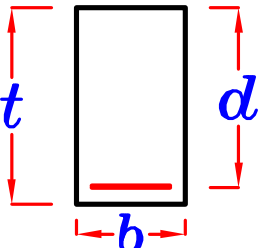
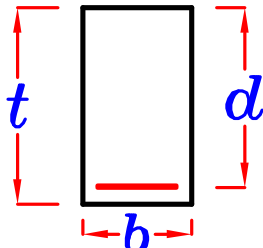
- ١- النظام القديم **Metric System** و نستخدم فيه **Ton, Kg, m & cm**
- ٢- النظام الحديث (**SI**) و هو حاليا النظام العالمي (**System International**) و يوجد نظام ثالث غير مستخدم في مصر لكن يستخدم في أوروبا و أمريكا يسمى (**British units or U.S. Customary units.**)

| |
|--------------------------------|
| kg = 9.81 N ≈ 10.0 N |
| ton = 9.81 kN ≈ 10.0 kN |

← للتحويل من **Metric System** الى **SI**

و الجدول التالي يوضح كيفية التحويل من النظام **Metric System** الى **SI** مع أمثله لتوضيح ذلك

| | Metric System | SI |
|-----------------------------|--|--|
| Concentrated Load | Kilogram (Kg) | Newton (N) |
| | 1 Kg ≈ 10 N | |
| | Ton (t) | kilo Newton (kN) |
| | 1 ton ≈ 10 kN | |
| Length | meter (m) | meter (m) |
| | centimeter (cm) | millimeter (mm) |
| | 1 cm = 10 mm | |
| Distributed Load (w) |  <p>w t/m² w (t/m²)</p> |  <p>w kN/m² w (kN/m²)</p> |
| | 1 t/m² = 10 kN/m² | |

| | <i>Metric System</i> | <i>SI</i> |
|---------------------------------------|--|--|
| Bending Moment (<i>M</i>) |  <p><i>M</i> (t.m) عند حساب الاحمال <i>M</i> (Kg.cm) فى معادلات التصميم</p> <p>لتحويل قيمه العزم من (t.m) الى (Kg.cm) يتم ضرب قيمه العزم فى 10^5</p> |  <p><i>M</i> (kN.m) عند حساب الاحمال <i>M</i> (N.mm) فى معادلات التصميم</p> <p>لتحويل قيمه العزم من (kN.m) الى (N.mm) يتم ضرب قيمه العزم فى 10^6</p> |
| | 1 t.m. = 10 kN.m | |
| | 1 Kg.cm = 100 N.mm | |
| Dimensions of sections. |  <p><i>b, d</i> & <i>t</i> (m) عند حساب الاحمال <i>b, d</i> & <i>t</i> (cm)</p> |  <p><i>b, d</i> & <i>t</i> (m) عند حساب الاحمال <i>b, d</i> & <i>t</i> (mm) فى معادلات التصميم</p> |
| | Area of Steel Bars (<i>A_s</i>) | |
| | cm² | mm² |
| | 1.0 cm² = 100 mm² | |
| | EX. 1 ∅ 16 ≈ 2.01 cm² ≈ 201 mm² | |
| Distributed | t/m² | kN/m² |
| Load at m² | 1 t/m² ≈ 10.0 kN/m² | |
| | EX. L.L. = 0.20 t/m² ≈ 2.0 kN/m² | |
| | EX. F.C. = 0.15 t/m² ≈ 1.50 kN/m² | |

| | <i>Metric System</i> | <i>SI</i> | | | | | | | | | | | | |
|--|--|---|-----|-----|-----|-----|-----|--|----|----|----|----|----|----|
| Stress | kg/cm^2 | $\text{N/mm}^2 = \text{MPa} = \text{Mega Pascal}$ | | | | | | | | | | | | |
| | $1 \text{ kg/cm}^2 \approx 0.10 \text{ N/mm}^2$ EX. $f_{cu} = 250 \text{ kg/cm}^2 \approx 25 \text{ N/mm}^2$ EX. $f_y = 3600 \text{ kg/cm}^2 \approx 360 \text{ N/mm}^2$ | | | | | | | | | | | | | |
| density | t/m^3 | kN/m^3 | | | | | | | | | | | | |
| | $1 \text{ t/m}^3 \approx 10.0 \text{ kN/m}^3$ EX. $\delta_c = 2.50 \text{ t/m}^3 \approx 25.0 \text{ kN/m}^3$ EX. $\delta_{wall} = 1.80 \text{ t/m}^3 \approx 18.0 \text{ kN/m}^3$ | | | | | | | | | | | | | |
| modules of Elasticity (E) | For Concrete $E_c = 14000 \sqrt{f_{cu}} \text{ (kg/cm}^2)$ | For Concrete $E_c = 4400 \sqrt{f_{cu}} \text{ (N/mm}^2)$ | | | | | | | | | | | | |
| | For Steel $E_s = 2 \times 10^6 \text{ (kg/cm}^2)$ | For Steel $E_s = 2 \times 10^5 \text{ (N/mm}^2)$ | | | | | | | | | | | | |
| المقاومه المميزه للخرسانه chrasaristics strength (f_{cu}) | $f_{cu} \text{ (kg/cm}^2)$ <table border="1" style="margin: 10px auto;"><tr><td>200</td><td>250</td><td>300</td><td>350</td><td>400</td><td>450</td></tr></table> | 200 | 250 | 300 | 350 | 400 | 450 | $f_{cu} \text{ (N/mm}^2) = \text{(MPa)}$ <table border="1" style="margin: 10px auto;"><tr><td>20</td><td>25</td><td>30</td><td>35</td><td>40</td><td>45</td></tr></table> | 20 | 25 | 30 | 35 | 40 | 45 |
| 200 | 250 | 300 | 350 | 400 | 450 | | | | | | | | | |
| 20 | 25 | 30 | 35 | 40 | 45 | | | | | | | | | |
| اجهاد الخضوع أو اجهاد الضمان للحديد yield stress or proof stress (f_y) | $f_y \text{ (kg/cm}^2)$ st. 24\35 $f_y = 2400 \text{ (kg/cm}^2)$ st. 36\52 $f_y = 3600 \text{ (kg/cm}^2)$ st. 40\60 $f_y = 4000 \text{ (kg/cm}^2)$ | $f_y \text{ (N/mm}^2) = \text{(MPa)}$ st. 240\350 $f_y = 240 \text{ (N/mm}^2)$ st. 360\520 $f_y = 360 \text{ (N/mm}^2)$ st. 400\600 $f_y = 400 \text{ (N/mm}^2)$ | | | | | | | | | | | | |

ملحوظه: تصميم القطاعات فى هذه الملفات بطريقه حالات الحدود L.S.D.M. Limits States Design Method

| | Metric System | SI |
|---|---|---|
| Design of section subjected to Bending Moment using First Principles | $0.67 \frac{f_{cu}}{\delta_c} a b = A_s \frac{f_y}{\delta_s}$ $M_{U.L.} = 0.67 \frac{f_{cu}}{\delta_c} a b \left(d - \frac{a}{2}\right)$ $M_{U.L.} = A_s \frac{f_y}{\delta_s} \left(d - \frac{a}{2}\right)$ | $0.67 \frac{f_{cu}}{\delta_c} a b = A_s \frac{f_y}{\delta_s}$ $M_{U.L.} = 0.67 \frac{f_{cu}}{\delta_c} a b \left(d - \frac{a}{2}\right)$ $M_{U.L.} = A_s \frac{f_y}{\delta_s} \left(d - \frac{a}{2}\right)$ |
| | Where: $a, b \text{ \& } d$ (cm) $A_s \text{ \& } A_c$ (cm ²) $f_{cu} \text{ \& } f_y$ (Kg/cm ²) $M_{U.L.}(\text{cm.Kg}) = M_{U.L.}(\text{m.t}) \times 10^5$ $A_{s \text{ min.}} = \frac{1.1}{f_y} A_c$ | Where: $a, b \text{ \& } d$ (mm) $A_s \text{ \& } A_c$ (mm ²) $f_{cu} \text{ \& } f_y$ (N/mm ²) $M_{U.L.}(\text{mm.N}) = M_{U.L.}(\text{m.KN}) \times 10^6$ $A_{s \text{ min.}} = \frac{11}{f_y} A_c$ |
| Design of section subjected to Bending Moment using Charts C₁ & J Chatr | $d = C_1 \sqrt{\frac{M_{U.L.}}{f_{cu} b}}$ $A_s = \frac{M_{U.L.}}{J f_y d}$ | $d = C_1 \sqrt{\frac{M_{U.L.}}{f_{cu} b}}$ $A_s = \frac{M_{U.L.}}{J f_y d}$ |
| | Where: $b \text{ \& } d$ (cm) $A_s \text{ \& } A_c$ (cm ²) $f_{cu} \text{ \& } f_y$ (Kg/cm ²) $M_{U.L.}(\text{cm.Kg}) = M_{U.L.}(\text{m.t}) \times 10^5$ $A_{s \text{ min.}} = \frac{1.1}{f_y} A_c$ | Where: $b \text{ \& } d$ (mm) $A_s \text{ \& } A_c$ (mm ²) $f_{cu} \text{ \& } f_y$ (N/mm ²) $M_{U.L.}(\text{mm.N}) = M_{U.L.}(\text{m.KN}) \times 10^6$ $A_{s \text{ min.}} = \frac{11}{f_y} A_c$ |

| | <i>Metric System</i> | <i>SI</i> |
|---|---|---|
| Design of section subjected to Compression Force only | $P_{U.L.} = 0.35 A_c f_{cu} + 0.67 A_s f_y$ | |
| | Where: $P_{U.L.}$ (Kg) A_c & A_s (cm ²) f_{cu} & f_y (Kg/cm ²) | Where: $P_{U.L.}$ (N) A_c & A_s (mm ²) f_{cu} & f_y (N/mm ²) |
| Design of section subjected to Tension Force only | $A_s = \frac{T_{U.L.}}{f_y / \delta_s}$ $A_c \approx (20 \rightarrow 40) A_s$ | |
| | Where: $T_{U.L.}$ (Kg) A_c & A_s (cm ²) f_y (Kg/cm ²) | Where: $T_{U.L.}$ (N) A_c & A_s (mm ²) f_y (N/mm ²) |
| Design of section subjected to Compression Force & Bending Moment $M_{U.L.}$ & $P_{U.L.}$ Tension Failure | $e = \frac{M_{U.L.}}{P_{U.L.}}$ $e_s = e + \frac{t}{2} - c$ $M_{su} = P_{U.L.} \times e_s$ $A_s = \frac{M_{su}}{J f_y d} - \frac{P_{U.L.}}{f_y / \delta_s}$ | |
| | Where: e, e_s, c, d & t (cm) $P_{U.L.}$ (Kg) $M_{su}(\text{cm.Kg}) = M_{su}(\text{m.t}) \times 10^5$ f_y (Kg/cm ²) A_s (cm ²) | Where: e, e_s, c, d & t (mm) $P_{U.L.}$ (N) $M_{su}(\text{mm.N}) = M_{su}(\text{m.KN}) \times 10^6$ f_y (N/mm ²) A_s (mm ²) |

| | Metric System | SI |
|--|--|--|
| Design of section subjected to Compression Force & Bending Moment $M_{U.L.}$ & $P_{U.L.}$ | $\frac{P_{U.L.}}{f_{cu} b t}, \quad \frac{M_{U.L.}}{f_{cu} b t^2}$ $\mu = \rho \times f_{cu} \times 10^{-5}$ $A_s = \mu d t$ $A_s' = \alpha A_s$ | $\frac{P_{U.L.}}{f_{cu} b t}, \quad \frac{M_{U.L.}}{f_{cu} b t^2}$ $\mu = \rho \times f_{cu} \times 10^{-4}$ $A_s = \mu d t$ $A_s' = \alpha A_s$ |
| Compression Failure using Interaction Diagram | Where: b & t (cm) $P_{U.L.}$ (Kg) $M_{U.L.}$ (cm.Kg) = $M_{U.L.}$ (m.t) $\times 10^5$ A_s (cm²) f_{cu} & f_y (Kg/cm²) | Where: b & t (mm) $P_{U.L.}$ (N) $M_{U.L.}$ (mm.N) = $M_{U.L.}$ (kN.m) $\times 10^6$ A_s (mm²) f_{cu} & f_y (N/mm²) |
| Check Shear | $q_u = \frac{Q_{U.L.}}{b d}$ $q_{cu} = 0.75 \sqrt{\frac{f_{cu}}{\delta_c}}$ $q_{u max} = 2.20 \sqrt{\frac{f_{cu}}{\delta_c}}$ $q_u - \frac{q_{cu}}{2} = \frac{n A_s (f_y / \delta_s)}{b S}$ $= \frac{n A_s}{b S} \geq \frac{0.4}{f_y}$ $\frac{A_{sb}}{b S} = \frac{q_{sub}}{(f_y / \delta_s) (\sin \alpha + \cos \alpha)}$ | $q_u = \frac{Q_{U.L.}}{b d}$ $q_{cu} = 0.24 \sqrt{\frac{f_{cu}}{\delta_c}}$ $q_{u max} = 0.70 \sqrt{\frac{f_{cu}}{\delta_c}}$ $q_u - \frac{q_{cu}}{2} = \frac{n A_s (f_y / \delta_s)}{b S}$ $= \frac{n A_s}{b S} \geq \frac{4.0}{f_y}$ $\frac{A_{sb}}{b S} = \frac{q_{sub}}{(f_y / \delta_s) (\sin \alpha + \cos \alpha)}$ |
| | Where: b & d (cm) $Q_{U.L.}$ (Kg) $q_u, q_{cu}, q_{u max}$ (Kg/cm²) A_s (cm²) f_{cu} & f_y (Kg/cm²) | Where: b & d (mm) $Q_{U.L.}$ (N) $q_u, q_{cu}, q_{u max}$ (N/mm²) A_s (mm²) f_{cu} & f_y (N/mm²) |

| | <i>Metric System</i> | <i>SI</i> |
|---|--|--|
| Check Shear + Torsion | $q_{tu} = \frac{M_{tu}}{2 A_o t_e}$ | |
| | $q_{tu} = \frac{M_{tu} (x_1 + y_1)}{0.85 (x_1^2 + y_1^2)} \quad \text{For R-sec.}$ | |
| | $q_{tu_{min}} = 0.19 \sqrt{\frac{f_{cu}}{\delta_c}}$ | $q_{tu_{min}} = 0.06 \sqrt{\frac{f_{cu}}{\delta_c}}$ |
| | $q_{tu_{max}} = 2.20 \sqrt{\frac{f_{cu}}{\delta_c}}$ | $q_{tu_{max}} = 0.70 \sqrt{\frac{f_{cu}}{\delta_c}}$ |
| $A_{str} = \frac{M_{tu} S_t}{1.7 x_1 y_1 (f_y / \delta_s)}$ | | |
| $A_{sl} = 2 A_{str} \frac{(x_1 + y_1)}{S_t} \left(\frac{f_{y_{str.}}}{f_{y_{L.b.}}} \right)$ | | |
| Where: | Where: | Where: |
| x_1, y_1 & S_t (cm) | x_1, y_1 & S_t (mm) | x_1, y_1 & S_t (mm) |
| M_{tu} (cm.Kg) | M_{tu} (mm.N) | M_{tu} (mm.N) |
| $q_{tu_{min}}, q_{tu_{max}}$ (Kg/cm ²) | $q_{tu_{min}}, q_{tu_{max}}$ (N/mm ²) | $q_{tu_{min}}, q_{tu_{max}}$ (N/mm ²) |
| A_{str}, A_{sl} (cm ²) | A_{str}, A_{sl} (mm ²) | A_{str}, A_{sl} (mm ²) |
| f_{cu} & f_y (Kg/cm ²) | f_{cu} & f_y (N/mm ²) | f_{cu} & f_y (N/mm ²) |

SI units → *U.S. Customary units*

يوجد حاليا في معظم دول العالم نوعان من الوحدات :

- النظام الحديث (*SI*) و هو حاليا النظام العالمى (*System International*) و يستخدم $^{\circ}\text{C}$ & mm , N و هذا هو النظام المستخدم في مصر حاليا .
- النظام الانجليزى و هو النظام الغالب ايضا في امريكا .
و يسمى (*British units or U.S. Customary units.*)
و يستخدم $^{\circ}\text{F}$ & in , lb

$$1 \text{ Kg} \approx 2.20 \text{ lb}$$

$$1 \text{ in} \approx 2.54 \text{ cm}$$

و الاسهل للتذكر

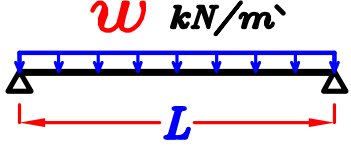
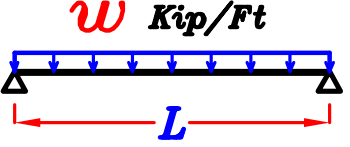


$$1 \text{ N} \approx 0.225 \text{ lb}$$

$$1 \text{ m} \approx 39.37 \text{ in}$$

للتحويل بين النظامين

و الجدول التالى يوضح كيفية التحويل من النظام *SI* الى *U.S. Customary*

| | <i>SI</i> | <i>U.S. Customary</i> |
|--------------------------|---|-------------------------|
| <i>Concentrated Load</i> | <i>Newton</i> (N) | <i>Pounds</i> (lb) |
| | $1 \text{ N} \approx 0.225 \text{ lb}$ | |
| | <i>kilo Newton</i> (kN) | <i>kilo Pound</i> (Kip) |
| | $1 \text{ kN} \approx 0.225 \text{ Kips}$ | |
| <i>Length</i> | <i>Meter</i> (m) | <i>Feet</i> (ft) |
| | $1 \text{ m} \approx 3.28 \text{ ft}$ | |
| | <i>centimeter</i> (cm) | <i>inch</i> (in) |
| | $1 \text{ cm} \approx 0.39 \text{ in}$ | |
| | $2.54 \text{ cm} \approx 1 \text{ in}$ | |
| | <i>Meter</i> (m) | <i>yard</i> (yd) |
| | $1 \text{ m} \approx 1.094 \text{ yd}$ | |

| | <i>SI</i> | <i>U.S. Customary</i> |
|---|---|---|
| Distributed Load (w) |  |  |
| | $1 \text{ N/m} \approx 0.068 \text{ lb/ft}$ | |
| | $1 \text{ kN/m} \approx 0.068 \text{ Kip/ft}$ | |
| Bending Moment (M) |  |  |
| | M (kN.m) عند حساب الاحمال M (N.mm) فى معادلات التصميم | M (Kip.ft) عند حساب الاحمال M (lb.in) فى معادلات التصميم |
| | $1 \text{ kN.m} \approx 0.737 \text{ Kip.ft}$ | |
| $1 \text{ N.m} \approx 8.85 \text{ lb.in}$ | | |
| Dimensions of sections. | b, d & t (m) عند حساب الاحمال | b, d & t (ft) عند حساب الاحمال |
| | $1 \text{ m} \approx 3.28 \text{ ft}$ | |
| | b, d & t (mm) فى معادلات التصميم | b, d & t (in) فى معادلات التصميم |
| $1 \text{ mm} \approx 0.04 \text{ ft}$ | | |
| Area of Steel Bars (A_s) | mm^2 | in^2 |
| | $1 \text{ mm}^2 \approx 0.00155 \text{ in}^2$ | |
| | الطريقه المستخدمه لتصنيف اقطار حديد التسليح مختلفه تماما فى النظام الامريكى . حيث الوحده تقاس بـ $(\frac{1}{8})$ بوصة | |
| $EX. 1\phi 16 \rightarrow \text{Diameter} = 16 \text{ mm}$ $A_s = \frac{\pi * 16^2}{4} = 201 \text{ mm}^2$ | $EX. *5 \rightarrow \text{Diameter} = \frac{5}{8} \text{ in}$ $A_s = \frac{\pi * (\frac{5}{8})^2}{4} = 0.306 \text{ in}^2$ | |
| Area Distributed Load | kN/m^2 | lb/in^2 |
| | $1 \text{ kN/m}^2 \approx 0.145 \text{ lb/in}^2$ | |

| | <i>SI</i> | <i>U.S. Customary</i> | | | | | | | | | | | | |
|--|---|---|------|------|------|----|----|--|------|------|------|------|------|------|
| Stress | $N/mm^2 = MPa = \text{Mega Pascal}$ | $Kips/in^2 = Ksi$ $lb/in^2 = Psi$ | | | | | | | | | | | | |
| | $1 N/mm^2 \approx 0.145 Ksi$ | | | | | | | | | | | | | |
| | $1 N/mm^2 \approx 145 Psi$ | | | | | | | | | | | | | |
| | EX. $f_{cu} = 25 N/mm^2 \approx 3625 Psi$ EX. $f_y = 360 N/mm^2 \approx 52.2 Ksi$ عند توصيف الحديد نوصفه بـ Ksi و عند توصيف الخرسانه نوصفها بـ Psi و فى جميع الاحوال يجب استخدام Psi فى معادلات التصميم | | | | | | | | | | | | | |
| Density | kN/m^3 | lb/ft^3 | | | | | | | | | | | | |
| | $1 kN/m^3 \approx 6.24 lb/ft^3$ | | | | | | | | | | | | | |
| | EX. $\delta_c = 25.0 kN/m^3 \approx 156 lb/ft^3$ EX. $\delta_{wall} = 18.0 kN/m^3 \approx 112 lb/ft^3$ | | | | | | | | | | | | | |
| modules of Elasticity (E) | For Concrete $E_c = 4400 \sqrt{f_{cu}} (N/mm^2)$ For Steel $E_s = 2 \times 10^5 (N/mm^2)$ | For Concrete $E_c = 33 * \delta_c * \sqrt{f_{cu}} (Psi)$ For Steel $E_s = 290 \times 10^5 (Psi)$ | | | | | | | | | | | | |
| | المقاومه المميزه للخرسانه <i>chrasaristics strength</i> (f_{cu}) | $f_{cu} (lb/in^2) = (Psi)$ | | | | | | | | | | | | |
| | <table border="1"> <tr> <td>20</td> <td>25</td> <td>30</td> <td>35</td> <td>40</td> <td>45</td> </tr> </table> | 20 | 25 | 30 | 35 | 40 | 45 | <table border="1"> <tr> <td>2900</td> <td>3625</td> <td>4350</td> <td>5075</td> <td>5800</td> <td>6525</td> </tr> </table> | 2900 | 3625 | 4350 | 5075 | 5800 | 6525 |
| 20 | 25 | 30 | 35 | 40 | 45 | | | | | | | | | |
| 2900 | 3625 | 4350 | 5075 | 5800 | 6525 | | | | | | | | | |
| اجهاد الخضوع أو اجهاد الضمان للحديد yield stress or proof stress (f_y) | $f_y (N/mm^2) = (MPa)$ | $f_y (N/mm^2) = (MPa)$ | | | | | | | | | | | | |
| | st. 240\350 $f_y = 240 (N/mm^2) \approx 34800 (Psi)$ | | | | | | | | | | | | | |
| | st. 360\520 $f_y = 360 (N/mm^2) \approx 52200 (Psi)$ | | | | | | | | | | | | | |
| | st. 400\600 $f_y = 400 (N/mm^2) \approx 58000 (Psi)$ | | | | | | | | | | | | | |

| | <i>SI</i> | <i>U.S. Customary</i> | | |
|---------------|--|---|-----------------------|-----------------------|
| Rebars | رقم السيخ هو قطر السيخ بال mm <i>EX. 1#16</i> → Diameter = 16 mm $A_s = \frac{\pi * 16^2}{4} = 201 \text{ mm}^2$ | رقم السيخ هو قطر السيخ بال in لكن مقسوم على 8 <i>EX. #5</i> → Diameter = $\frac{5}{8}$ in $A_s = \frac{\pi * (\frac{5}{8})^2}{4} = 0.306 \text{ in}^2$ | | |
| | ϕ | A_s | $\#$ | A_s |
| | $\phi 6$ | 28.2 mm ² | $\# 2$ | 0.049 in ² |
| | $\phi 8$ | 50.3 mm ² | $\# 3$ | 0.110 in ² |
| | $\phi 10$ | 78.5 mm ² | $\# 4$ | 0.196 in ² |
| | $\phi 12$ | 113 mm ² | $\# 5$ | 0.306 in ² |
| | $\phi 16$ | 201 mm ² | $\# 6$ | 0.441 in ² |
| | $\phi 18$ | 254 mm ² | $\# 7$ | 0.601 in ² |
| | $\phi 20$ | 314 mm ² | $\# 8$ | 0.785 in ² |
| | $\phi 22$ | 380 mm ² | $\# 9$ | 0.994 in ² |
| | $\phi 25$ | 490 mm ² | $\# 10$ | 1.227 in ² |
| | $\phi 28$ | 615 mm ² | $\# 11$ | 1.485 in ² |
| $\phi 32$ | 804 mm ² | $\# 12$ | 1.767 in ² | |